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### (54) Power supply unit for automotive vehicle

(57) A Zener diode 16 is connected to each of single cells 10 of an electric double layer capacitor in parallel, and a resistor 18 is connected to each of the Zener diode 16 in series. Thus, in a case where a single cell 10 is excessively charged, when the bias voltage of the single cell 10 is equal to or higher than the Zener voltage, a discharge current flows through the Zener diode 16

connected to the single cell 10, so that the voltage decreases to the Zener voltage. Thus, it is possible to prevent the electric double layer capacitor from being excessively charged due to the dispersions in electrostatic capacity and internal resistance, and to stably accumulate electricity for a long time.

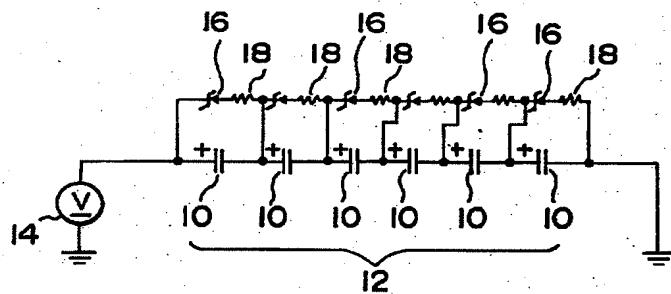


FIG. 3

EP 0 795 947 A2

**Description****BACKGROUND OF THE INVENTION**

The present invention relates generally to a power supply unit for automotive vehicles. More specifically, the invention relates to a power supply for feeding electric current to various electrical loads of an automotive vehicle.

In recent years, it has been proposed to use an electric double layer capacitor, the capacity of which is remarkably increased using an electric double layer structure of electrons produced on the interface between electrodes and an electrolyte, as a cell. This electric double layer capacitor generates a voltage of, e.g., about 2.5V, as a single cell. Therefore, in a case where this electric double layer capacitor is used for a power supply unit for an automotive vehicle, a plurality of single cells 100 are connected in series to be used as a capacitor pack as shown in FIG. 1.

That is, each of the single cells 100 is formed as an electric double layer capacitor which comprises a pair of current collecting bodies, each having an active carbon electrode, an electrolyte charged between the current collecting bodies, and a separator for separating the active carbon electrodes of the respective current collecting bodies from each other (all the elements are not shown). These single cells 100 are connected in series to form a capacitor pack 102. The capacitor pack 102 is connected to an on-vehicle generator 104 mounted on the vehicle. The on-vehicle generator 104 generates a voltage according to engine rotation, and the generated voltage is converted into a DC voltage by means of a rectifier to be output. Specifically, an alternator corresponds to the on-vehicle generator 104.

During the engine is operated, each of the single cells 100 is charged by the DC voltage from the on-vehicle generator 104, and the stored energy is discharged and used to drive a starter motor when the engine is restarted, and so forth.

The electromotive force of each of the single cells 100 is determined by the active voltage of the electrolyte. When a bias voltage, i.e., a charging voltage from the on-vehicle generator 104, exceeds the active voltage, the life time of the single cell 100 of electric double layer capacitor is rapidly decreased. In view of a margin of the safety, if the rated voltage of each of the single cells 100 is set to be lower than the active voltage of the electrolyte and if the single cells 100 are used at a voltage equal to or less than the rated voltage, it is possible to ensure a long life time which is one of characteristics of the electric double layer capacitor.

However, the dispersions in electrostatic capacity and internal resistance of the single cells 100 may occur. Therefore, if the single cells 100 are charged from the on-vehicle generator 104 while being connected in series, the difference between the bias voltages may occur due to the dispersions in electrostatic capacity and internal resistance. That is, in a case

where the single cells 100 are connected in series to be charged, if the electrostatic capacities and the values of internal resistance of the respective single cells are the same, the terminal-to-terminal voltages (the bias voltages) of the respective single cells are also the same. However, if there are the dispersions in electrostatic capacity and internal resistance, the imbalance in bias voltage occurs between the respective single cells. In addition, this difference in bias voltage may be integrated and increased when charge and discharge are repeatedly carried out.

Therefore, if the rated voltage is set in view of a margin of the safety, a higher bias voltage than the rated voltage may be impressed on one of the single cells 100 due to the dispersion in characteristics of the respective single cells 100, which may cause to decrease the life time.

In order to overcome such a problem, a "balance circuit system" has been adopted. As shown in FIG. 2, this system is designed to balance the bias voltages of the respective single cells 100 by connecting balance resistors 106 having the same resistance to the respective single cells 100 via resistors 108 in parallel for every single cells 100 and by connecting the respective balance resistors 106 in series.

In addition, Japanese Utility Model Laid-Open No. 5-23527 discloses another conventional system wherein a balance resistor is electrically separated from a single cell when no charge is carried out, and the single cell and the balance resistor are connected in parallel when the terminal-to-terminal voltage of the single cell is higher than a predetermined value.

In the aforementioned conventional balance circuit system wherein the balance resistors 106 are connected to the respective single cells 100 in parallel, it is possible to equalize the bias voltages applied to the respective single cells 100, since the divided voltages are the same if the values of resistance of the respective balance resistors 106 are the same.

However, in the case of the balance circuit system, since the balance resistors 106 are always connected to the respective single cells 100 so that the whole electric circuit forms a closed loop, the electric energies stored in the respective single cells 100 are gradually lost as the discharge is carried out. Therefore, this system can not function as a "battery" since the discharge of each of the single cells 100 are started after the charge is stopped, so that this system can not be practically used as a power supply unit for driving, e.g., a starter motor, which is used when the engine is restarted, of an automotive vehicle.

In order to overcome this problem, in the aforementioned system disclosed in Japanese Utility Model Laid-Open No. 5-23527, the balance resistors are selectively connected to the single cells in parallel and separated therefrom by means of transistors and so forth. According to this system, it is possible to prevent the discharge to store the electric energy for a long time, since the balance resistors are separated from the single cells when

no charge is carried out. However, according to this system, there are other problems in that the circuit structure is not only complicated due to the additional switch circuit to increase the manufacturing costs, but the reliability is also decreased due to the increase of the number of parts.

The aforementioned problems on the balance circuit system also appear in a lead battery pack used for a power supply unit of an electric vehicle. This lead battery pack is made by connecting a plurality of single cells like the capacitor pack shown in Figs. 1 and 2.

### SUMMARY OF THE INVENTION

It is therefore an object of the present invention to eliminate the aforementioned problems and to provide a power supply unit using cells of electric double layer capacitors or lead battery for an automotive vehicle, which can balance the bias voltages of the cells with a simple structure and which can control the discharge even if no charge is carried out.

In order to accomplish the aforementioned and other objects, according to one aspect of the present invention, a power supply unit for an automotive vehicle, comprises: a battery cell connected to an on-vehicle generator; a Zener diode connected to the battery cell in parallel in a direction that a reverse bias voltage is impressed thereon; and a resistor connected to the Zener diode in series. Thus, in a case where the bias voltage of the battery cell is equal to or higher than the Zener voltage, the discharge of the cell is permitted and a current defined by the resistance value of the resistor flows through the Zener diode, so that the bias voltage of the battery cell decreases to the Zener voltage. On the other hand, in a case where the bias voltage of the battery cell is less than the Zener voltage, the discharge is not permitted, so that the electric energy is conserved except for a slight self-discharge. Therefore, even if there are dispersions in electrostatic capacity and internal resistance, it is possible to maintain the bias voltage of the battery cell at a constant value to prevent the life time thereof from decreasing.

Another diode may be added to the Zener diode. In this case, it is possible to carry out the fine adjustment of the threshold for permitting the discharge.

In place of the Zener voltage, the forward threshold voltage of the diode may be utilized. In this case, the discharge is not permitted at a voltage less than the forward threshold voltage, and the discharge is carried out at a voltage equal to or higher than the forward threshold voltage. Therefore, it is possible to balance the bias voltages while preventing useless discharge.

The diode may be a light emitting diode. In this case, since the light emitting diode for adjusting the bias voltage by discharge emits light, it is possible to easily visually recognize the charged state of the electric double layer capacitor from the outside.

As mentioned above, a power supply unit using a battery cell for an automotive vehicle, according to the

present invention, is designed to permit the discharge from the battery cell when the bias voltage of the battery cell is equal to or higher than the Zener diode, and to stop the discharge when the bias voltage of the battery cell decreases to the Zener diode. Therefore, it is possible to effectively prevent the excessive charge of the battery cell and to prevent useful discharge to maintain the battery function for a long time, so that it is possible to improve the practicability.

In addition, when the light emitting diode is utilized, it is possible to confirm the charged state of the battery cell, wherein the bias voltage is adjusted, without the need of any measuring instruments, so that it is possible to improve the maintenance. Moreover, when the unit is formed so that the battery cell is charged at a charging voltage which is not greater than the rated voltage of the battery cell and which is equal to or greater than the Zener voltage, it is possible to more suitably adjust the balance of the voltages of the battery cells when the engine is operated.

### BRIEF DESCRIPTION OF THE DRAWINGS

In the drawings:

FIG. 1 is a schematic circuit diagram illustrating a main part of a conventional power supply unit using electric double layer capacitors for an automotive vehicle;

FIG. 2 is a schematic circuit diagram illustrating a conventional balance circuit system;

FIG. 3 is a schematic circuit diagram illustrating a main part of the first preferred embodiment of a power supply unit using electric double layer capacitors for an automotive vehicle according to the present invention;

FIG. 4 is a graph explaining the electrical characteristic of a Zener diode;

FIG. 5 is a schematic circuit diagram illustrating a main part of the second preferred embodiment of a power supply unit using electric double layer capacitors for an automotive vehicle according to the present invention;

FIG. 6 is a graph explaining the electrical characteristic of a diode;

FIG. 7 is a schematic circuit diagram illustrating a main part of the third preferred embodiment of a power supply unit using electric double layer capacitors for an automotive vehicle according to the present invention;

FIG. 8 is a schematic circuit diagram illustrating a main part of the fourth preferred embodiment of a power supply unit using electric double layer capacitors for an automotive vehicle according to the present invention;

FIG. 9 is a schematic circuit diagram illustrating a main part of the fifth preferred embodiment of a power supply unit using electric double layer capacitors for an automotive vehicle according to the

present invention;

FIG. 10 is a schematic circuit diagram illustrating a main part of the sixth preferred embodiment of a power supply unit using electric double layer capacitors for an automotive vehicle according to the present invention;

FIG. 11 is a schematic circuit diagram illustrating a main part of the seventh preferred embodiment of a power supply unit using electric double layer capacitors for an automotive vehicle according to the present invention; and

FIG. 12 is a schematic circuit diagram illustrating a main part of the eighth preferred embodiment of a power supply unit using electric double layer capacitors for an automotive vehicle according to the present invention.

#### DESCRIPTION OF THE PREFERRED EMBODIMENT

Referring now to the accompanying drawings, particularly to FIGS. 3 through 12, the preferred embodiments of the present invention will be described in detail below.

FIG. 3 shows a circuit of the first preferred embodiment of a power supply unit using electric double layer capacitors for an automotive vehicle according to the present invention.

Each of single cells 10 of an electric double layer capacitor comprises, e.g., a pair of current collecting bodies, each having an active carbon electrode on the surface thereof, an electrolyte charged between the current collecting bodies, a separator provided between the active carbon electrodes so as to separate the electrodes from each other, and a gasket for preventing the leakage of the electrolyte (all the elements are not shown). These single cells 10 are designed to be connected in series to form a capacitor pack 12 which generates a desired electromotive force.

The positive side of the capacitor pack 12, thus formed by connecting the single cells 10 in series, is connected to an on-vehicle generator 14, and the negative side thereof is grounded. The on-vehicle generator 14 outputs a DC voltage rectified by a rectifier, and generates a voltage according to engine rotation.

A Zener diode 16 for limiting a bias voltage is connected to each of the single cells 10 in parallel. A resistor 18 is connected to each of the Zener diodes 16 in series for each of the single cells 10. The circuits, each comprising the single cell 10, the Zener diode 16 and the resistor 18, are connected in series.

The cathode terminal of each of the Zener diodes 16 is designed to be connected to the corresponding single cell 10. As shown in FIG. 4, the Zener diode 16 is an active element which allows current to flow from the cathode side to the anode side when a reverse bias voltage  $-VB$  greater than a predetermined Zener voltage  $VZ$  is impressed. Therefore, the Zener diode 16 allows current supply only when a reverse bias voltage  $-VB$  greater than the Zener voltage  $VZ$  is impressed.

In addition, each of the Zener diodes 16 is preferably set so that the Zener voltage  $VZ$  is equal to or slightly less than the rated voltage of the single cell 10. In a case where the Zener diode  $VZ$  is less than the rated voltage of the single cell 10, the difference between the rated voltage and the Zener voltage  $VZ$  is a margin for the safety. Moreover, Zener diodes having a small rated power, e.g., a rated power of about 1W, are selected as the Zener diodes 16. Furthermore, in FIG. 4, while a negative sign is applied to the reverse bias voltage  $VB$  to distinguish the reverse bias voltage from the forward bias voltage  $VB$ , the sign "VB" will be hereinafter applied to the reverse bias voltage.

Each of the resistors 18 is designed to limit the value of discharge current  $I$  passing through the corresponding Zener diode 16 when the bias voltage  $VB$  of the corresponding single cells 10 exceeds the Zener voltage  $VZ$ . In accordance with the capacity of the Zener diode 16, the resistance of each of the resistors 18 is preferably set so that the discharge current is as small as possible.

With this construction, the operation of this preferred embodiment will be described below.

When the engine is started, the on-vehicle generator 14 outputs a predetermined discharging voltage. The bias voltages  $VB$  impressed on the respective single cells 10 are different from each other due to the dispersions in electrostatic capacity and internal resistance.

For example, when only the bias voltage  $VB$  of a particular single cell 10 increases to exceed the Zener diode voltage  $VZ$ , the Zener diode 16 connected to the single cell 10 in parallel allows current to pass therethrough, so that a predetermined discharge current  $I$  limited by the resistor 18 flows. Then, since the bias voltage  $VB$  decreases by this discharge current  $I$ , an excessive bias voltage  $VB$  of the single cell 10 is coincident with the Zener diode  $VZ$ , so that the discharge is stopped.

On the other hand, in a single cell 10 wherein the bias voltage  $VB$  is less than the Zener voltage  $VZ$ , the Zener diode connected to the single cell 10 in parallel is not actuated, so that the discharge current  $I$  does not flow. With this construction, this preferred embodiment has the following advantageous effects.

First, each of the Zener diodes 16 is connected to the corresponding single cell 10 of an electric double layer capacitor in parallel, and each of the resistors 18 is connected to the corresponding Zener diodes 16 in series, so that it is possible to prevent the excessive charge due to the difference in electrostatic capacity and internal resistance by setting the Zener voltage  $VZ$  at a value near the rated voltage of the corresponding single cells 10. Therefore, it is possible to prevent the excessive charge that excessive bias voltage  $VB$  is impressed on the single cell, so that it is possible to prevent the life time from decreasing.

In addition, in a case where the bias voltage  $VB$  of the single cell 10 decreases to the Zener voltage  $VZ$  or

in a case where the original bias voltage  $VB$  is less than the Zener voltage  $VZ$ , the operation of the Zener diode 16 is stopped, so that the discharge is not carried out. Therefore, it is possible to prevent useless discharge to maintain the charge stored in the single cell for a long time, so that it is possible to surely supply a large and stable current when a starter is driven and so forth.

Second, since the rated power of the Zener diode 16 is set at a value as small as possible, e.g., 1 W, it is possible to decrease the calorific value of the Zener diode 16 when the single cell 10 discharges to adjust the bias voltage  $VB$ . Therefore, it is not required to add a radiation mechanism, such as a cooling fin, to the Zener diode 16, so that it is possible to decrease the size of the whole circuit without increasing the number of parts and the manufacturing costs.

Third, since the resistance values of the respective resistors are set so that the discharge current  $I$  is as small as possible in view of the rated capacity of the Zener diode 16, it is possible to decrease the costs of the resistors 18. On the other hand, in a case where the discharge current  $I$  is set to be a large value, the bias voltage  $VB$  quickly decreases to the Zener voltage  $VZ$ , so that it is possible to decrease the time required to adjust the bias voltage. However, since the calorific value of the resistor 18 increases due to the increase of the discharge current  $I$ , an expensive resistor having a large rated power must be used as the resistor 18.

In addition, unless the single cell 10 deteriorates due to the excessive charge, there is no problem if it takes a lot of time to adjust the bias voltage. Therefore, unless there are problems on the decrease of life time of the single cell 10, it is possible to prevent the excessive charge at a low cost using the resistors 18 which require a long period of time to adjust the bias voltage. However, the present invention also includes a unit wherein the resistors 18 of relatively larger resistance value are used to decrease the period of time required to adjust the bias voltage.

Referring to FIGS. 5 and 6, the second preferred embodiment of the present invention will be described below. Furthermore, in the undermentioned preferred embodiments, the same signs will be used for the same elements as those in the aforementioned first preferred embodiment, and the descriptions thereof will be omitted.

FIG. 5 shows a circuit of the second preferred embodiment of a power supply unit using electric double layer capacitors for an automotive vehicle. Also in this preferred embodiment, single cells 10 of an electric double layer capacitor are connected in series to form a capacitor pack 12 which is connected to an on-vehicle generator 14.

The feature of this preferred embodiment is that diodes 20 are used for the respective single cells 10 in place of the Zener diodes 16 in the aforementioned first preferred embodiment. A resistor 22 for limiting a discharge current  $I$  is connected to each of the diodes 22 in series. Furthermore, the rated power of each of the

diodes 20 is preferably small. Each of the resistors 22 is also set so that the discharge current is small.

The anode terminal of each of the diodes 20 is connected to the positive electrode terminal of the corresponding single cell 10. As shown in FIG. 6, each of the diodes 20 allows the forward current to pass therethrough when the forward bias voltage  $VB$  exceeds a predetermined threshold voltage  $VF$ .

Therefore, each of the diodes 20 does not allow the discharge current  $I$  to pass therethrough unless the bias voltage  $VB$  reaches the forward bias threshold voltage  $VF$ , so that the discharge of each of the single cell 10 is not carried out. On the other hand, when the bias voltage  $VB$  decreases to the threshold voltage  $VF$  during the discharge of the single cells 10, the discharge is stopped. Furthermore, a slight current flows through each of the diodes 20 if the bias voltage  $VB$  is less than the forward bias threshold voltage  $VF$ . In the case of the Zener diodes 16, a slight current also flows therethrough when the bias voltage  $VB$  is less than the Zener voltage  $VZ$ . However, these current values are very small, so that it is possible to practically ignore these currents.

With this construction, in this preferred embodiment, the bias voltage  $VB$  is adjusted by the forward bias threshold voltage  $VF$  of the diode 20, so that it is possible to prevent the excessive charge caused by electrostatic capacity and internal resistance and to improve the life time, similar to the aforementioned first preferred embodiment. In addition, since the discharge is stopped immediately after the bias voltage  $VB$  decreases to the threshold voltage  $VF$  by the discharge, it is possible to prevent useless discharge to maintain the voltage for a long time, and to ensure an effective current supply if necessary, e.g., when the engine is started. In particular, since the forward bias threshold voltage  $VF$  of the diode 20 is generally less than the Zener voltage  $VZ$  (for example, from 0.3 to 0.4V in the case of germanium, from 0.7 to 1.0V in the case of silicon), this unit can be suitably used when the rated voltage of each of the single cells 10 is too low to utilize the Zener voltage  $VZ$  of the Zener diode 16.

Referring to FIG. 7, the third preferred embodiment of the present invention will be described below.

As shown in the schematic circuit diagram of FIG. 7, the third preferred embodiment of a power supply unit using electric double layer capacitors for an automotive vehicle, according to the present invention, comprises a capacitor pack 12, which is formed by connecting single cells 10 of an electric double layer capacitor in series and which is connected to an on-vehicle generator 14, similar to the aforementioned second preferred embodiment.

A light emitting diode 30 substituted for the diode 20 in the aforementioned second preferred embodiment, is connected to each of the single cells in parallel. Similar to the aforementioned preferred embodiment, a resistor 32 for limiting a discharge current  $I$  is connected to each of the light emitting diodes 30 in series. Furthermore,

the rated power of each of the light emitting diodes 30 is preferably as small as possible. The resistor 32 is also set so that the discharge current  $I$  is small.

Similar to the diode 20 used in the aforementioned second preferred embodiment, the anode terminal of each of the light emitting diodes 30 is connected to the positive electrode terminal, so that each of the light emitting diodes 30 allows a forward current to pass therethrough to emit light in accordance with the magnitude of the forward current, i.e., the discharge current  $I$ , when the forward bias voltage  $VB$  exceeds a predetermined threshold voltage  $VF$ .

Therefore, until the bias voltage  $VB$  reaches the forward threshold voltage  $VF$ , the light emitting diode 30 does not allow the discharge current  $I$  to pass therethrough, so that the discharge of the single cell 10 is not carried out. In addition, when the bias voltage  $VB$  decreases to the threshold voltage  $VF$ , the discharge is stopped by the light emitting diode 30. Moreover, the luminance of the light emitting diode 30 decreases as the discharge current  $I$  decreases, and it increases as the discharge current  $I$  increases.

Thus, in this preferred embodiment, it is possible to suitably control the permission and stop of the discharge of each of the single cells 10, and to visually recognize the control state from the outside. That is, a light emitting diode 30 connected to a single cell 10 in parallel, which is in danger of excessive charge, emits light immediately after the adjustment of the bias voltage  $VB$  by the discharge is started. On the other hand, in a case where the bias voltage  $VB$  is a normal value or in a case where the bias voltage  $VB$  is low due to the lack of discharge, a light emitting diode 30 connected to a corresponding cell 10 in parallel does not emit light since the discharge current  $I$  does not flow. Therefore, it is possible to easily recognize the charged state of the single cell 10 from the outside on the basis of the presence of emission and luminance of the light emitting diode 30, without the need of any measuring instruments, so that it is possible to improve the maintenance. Furthermore, similar to the aforementioned preferred embodiments, it is possible to prevent the excessive charge due to electrostatic capacity and internal resistance, and to prevent the life time for decreasing.

Referring to the circuit diagram of FIG. 8, the fourth preferred embodiment of the present invention will be described below.

In this preferred embodiment of a power supply unit for an automotive vehicle according to the present invention, a plurality of single cells 10 of an electric double layer capacitor are connected in series to form a combination cell 40, and a plurality of combination cells 40 thus formed are connected in series to form a capacitor pack 42. For each of the combination cells 40, a circuit is formed by connecting a Zener diode 44, a light emitting diode 46 and a resistor 48 in series to each other and in parallel to the combination cell 40, and a plurality of circuits thus formed are connected in series to form the whole circuit.

In this preferred embodiment, since the Zener diode 44 and the light emitting diode 46 are connected in series, when a bias voltage  $VB$  is equal to or higher than a total value of a Zener voltage  $VZ$  and a forward bias threshold voltage  $VF$  ( $VB \geq VZ + VF$ ), a discharge current  $I$  flows to start the voltage adjustment. Furthermore, in this preferred embodiment, since the Zener diode 44 and the light emitting diode 46 are connected, in parallel, to the combination cell 40 formed by connecting, e.g., three single cells 10, the bias voltage  $VB$  is higher than that in the aforementioned preferred embodiments wherein the active element is connected to each of the single cells 10 in parallel.

In this preferred embodiment of such a construction, the adjustment of the bias voltage is carried out for each of the combination cells 40 formed by connecting the plurality of single cells 10 in series, not for each of the single cells 10. However, similar to the aforementioned preferred embodiments, it is possible to prevent the excessive charge of the combination cell 40 by the discharge permitted by the Zener diode 44 and the light emitting diode 46. In addition, it is possible to suppress useless discharge to conserve electric energy for a long time, and to enhance the practicability. Moreover, since the luminance of the light emitting diode 46 varies in accordance with the magnitude of the discharge current  $I$ , it is possible to easily visually recognize the charged state from the outside.

In addition, in this preferred embodiment, as mentioned above, it is possible to determine the discharge starting voltage as the total value of the Zener voltage  $VZ$  of the Zener diode 44 and the forward bias threshold voltage  $VF$  of the light emitting diode 46, and it is possible to accurately carry out the voltage adjustment for the excessive charge. Therefore, while it has been explained that one light emitting diode 46 is connected to the Zener diode 44 in series, the present invention should not be limited thereto. For example, two light emitting diodes 46 may be connected to the Zener diode 44. Alternatively, the light emitting diode 46 and a usual diode are connected to the Zener diode 44 to set the discharge starting voltage.

In addition, in this preferred embodiment, if it is set so that the temperature characteristic of the Zener diode 44 is coincident with the temperature characteristic of the light emitting diode 45, i.e., so that one characteristic variation due to temperature variation is canceled out by the other characteristic variation due to temperature variation, it is possible to accurately adjust the voltage for the excessive charge regardless of the temperature variation.

Referring to FIG. 9, the fifth preferred embodiment of the present invention will be described below.

FIG. 9 is a circuit diagram illustrating an enlarged main portion of an electric circuit of a power supply unit for an automotive vehicle according to the present invention. In this preferred embodiment, single cells 10 of an electric double layer capacitor are connected in series to form a capacitor pack 12 which is connected to

an on-vehicle generator 14 (not shown) similar to the aforementioned preferred embodiments.

A light emitting diode 50 is connected to each of the single cells 10 in parallel, and a resistor 52 for defining a discharge current  $I$  is connected to each of the light emitting diodes 50. A phototransistor 54 serving as a light receiving element, which receives light emitted by the light emitting diode 50 to convert the light into a voltage signal, is provided near the light emitting diode 50.

That is, the light emitting diode 50 and the phototransistor 54 form a photocoupler 56 as a whole. The collector terminal of each of the phototransistors 54 is connected to a monitor 58. The monitor 58 displays the voltage adjusted states of the respective single cells 10 on the basis of the voltage signals from the phototransistors 54. For example, the monitor 56 comprises a display section such as a LED display, a LED lamp and a meter, an input interface circuit and so forth.

In this preferred embodiment, the light emitted state of the light emitting diode 50 is detected by means of the phototransistor while being electrically insulated, and the detected results are output to the monitor 58, so that it is possible to confirm the voltage adjusted state of the single cell 10 by means of the monitor 58. Furthermore, the light emitting diode 50 serving as a charging voltage detecting section is electrically insulated from the monitor 58 serving as a luminous-state detecting section. Therefore, it is not required to provide any special elements such as an insulating rubber, so that it is possible to safely and easily monitor the charged states of the respective single cells 10 without being in danger of an electric shock.

This preferred embodiment also has the same advantageous effects as those of the aforementioned preferred embodiments, since the discharge is stopped when the bias voltage  $VB$  decreases to the forward bias threshold voltage  $VF$  of the light emitting diode 50.

In particular, similar to the fourth preferred embodiment described referring to FIG. 8, in a case where a plurality of single cells 10 are connected in series to form a combination cell 40 to determine whether the excessive charge occurs for each of the combination cells 40, it is effective to monitor using the insulation of the photocoupler 56, since the terminal-to-terminal voltage of the combination cell 40, i.e., the bias voltage  $VB$ , increases by the single cells 10 connected in series.

Referring to FIG. 10, the sixth preferred embodiment of the present invention will be described below.

This preferred embodiment is characterized by the setting of a voltage value when each of single cells 10 is charged. That is, FIG. 10 is a circuit diagram of this preferred embodiment of a power supply unit for an automotive vehicle according to the present invention, and this electric circuit has basically the same construction as that of the first preferred embodiment shown in FIG. 1.

However, in this preferred embodiment, the charging voltage output from an on-vehicle generator 60 is set so as to exceed the rated voltage of the single cell 10

and to be equal to or higher than the total Zener voltage  $VZ$  of Zener diodes 16. That is, assuming that the Zener voltages  $VZ$  of the Zener diodes 16 are  $VZ1, VZ2, \dots, VZN$ , the on-vehicle generator 60 serving as a DC constant-voltage source mounted on the vehicle outputs a voltage equal to or higher than the total Zener voltage  $VZT (=VZ1+VZ2+\dots+VZN)$ .

Thus, in a case where the bias voltage  $VB2$  of a single cell  $CB2$  of the single cells (CB) 10 in FIG. 8 is higher than the Zener voltage  $VZ2$ , a discharge current flows through the Zener diode 16 connected to the single cell  $CB2$  in parallel. Since the on-vehicle generator 60 is a constant-voltage source, it supplies a current corresponding to the discharge current. The current supplied from the on-vehicle generator 60 is supplied to all the single cells  $CB1, CB2, \dots, CBN$  connected in series. As a result, single cells having a lower bias voltage than that of the single cell  $CB2$  are charged by the current from the on-vehicle generator 60, so that the bias voltages thereof increase.

Therefore, the voltages of excessively charged single cells, to which a bias equal to or higher than the rated voltage (Zener voltage  $VZ$ ) is applied, are decreased by discharge, and the voltages of insufficiently charged single cells, to which a bias less than the rated voltage, are increased by charge. Thus, it is possible to balance the charging voltages of the single cells 10 even if the engine is operated.

That is, in the aforementioned preferred embodiments, the excessively charged single cells 10 are discharged during the voltage output from the on-vehicle generator 14 is stopped due to the stop of the engine, so that it is possible to balance the voltages of the single cells to prepare to carry out a new charge by the restart of the engine.

In this case, the voltages of the excessively charged single cells 10 are decreased to the Zener voltage  $VZ$  by discharge, and the discharge current  $I$  is supplied to the other insufficiently charged single cells 10. However, in a case where the number of the insufficiently charged single cells 10 are great or the amount of insufficiency (the difference from the Zener voltage  $VZ$ ) is great, the voltages of the insufficiently charged single cells 10 may not be increased to the Zener voltage  $VZ$ .

On the other hand, in this preferred embodiment, the charged voltage output from the on-vehicle generator 60 serving as a constant-voltage source during the operation of the engine is set at a value equal to or higher than the total Zener diode  $VZ$  of the Zener diodes 16, each of which is connected to each of the single cells 10 in parallel. Therefore, it is possible to increase the bias voltages of the insufficiently charged single cells 10 while decreasing the bias voltages of the excessively charged single cells 10, so that it is possible to effectively recover and maintain the whole balance.

Referring to FIG. 11, the seventh preferred embodiment of the present invention will be described below.

As shown in the circuit diagram of FIG. 11, this pre-

ferred embodiment of a power supply unit for an automotive vehicle is characterized in that variable resistors 70 are substituted for the resistors 18 in the aforementioned first preferred embodiment. Each of these variable resistors 70 can variably adjust the resistance value thereof, e.g., by rotating a trimmer provided thereon.

This preferred embodiment has the same advantageous effects as those in the aforementioned first preferred embodiment. In addition, since the resistance value is variable to define the discharge current I, it is possible to set the resistance at a desired value in accordance with the dispersions in electrostatic capacity of the single cells 10. Moreover, even if the characteristic of the single cell 10 varies with time, it is possible to limit the discharge current I in accordance with the characteristic variation, so that it is possible to improve the usability and reliability.

Referring to FIG. 12, the eighth preferred embodiment of the present invention will be described below.

In this preferred embodiment of a power supply unit for an automotive vehicle according to the present invention, as shown in FIG. 12, a plurality of single cells 10 are connected in series to form a combination cell 80, and a plurality of combination cells 80 thus formed are connected in series to form a capacitor pack 82. A Zener diode 84 is connected to each of the combination cells 80 in parallel, and a resistor 86 is connected to each of the Zener diodes 84 in series. With this construction, according to this preferred embodiment, it is possible to set the voltage for preventing the excessive charge for each of the combination cells 80.

Furthermore, the present invention should not be limited to the aforementioned preferred embodiments, but the present invention can be embodied in various ways without departing from the principle of the invention. For example, the described constructions can be suitably combined, and the number of the single cells can be changed. And, importantly, each of the circuits described in Figs. 3 through 12 can be applied to a lead battery pack for an electric vehicle. The same explanation can be made except for replacing capacitor cells with lead battery cells.

While the presently preferred embodiments of the present invention have been shown and described, it is to be understood that this disclosure is for the purpose of illustration and that various changes and modifications may be made without departing from the scope of the invention as set forth in the appended claims.

#### Claims

1. A power supply unit for an automotive vehicle, said power supply unit comprising:

a battery mounted on the vehicle to feed electric current to various electrical loads and connected so as to be capable of being charged from an on-vehicle generator;

a Zener diode connected to said battery in par-

allel in a direction that a reverse bias voltage is impressed thereon; and  
a resistor connected to said Zener diode in series.

5. 2. A power supply unit as set forth in claim 1, wherein said battery is charged by a charging voltage which is equal to or less than a rated voltage of said battery and which is higher than a Zener voltage of said Zener diode.

10 3. A power supply unit as set forth in claim 1, which further comprises a diode connected to said Zener diode in a direction that a forward bias voltage is impressed thereon.

15 4. A power supply unit for an automotive vehicle, said power supply unit comprising:

20 a battery mounted on said vehicle to feed electric current to various electrical loads and connected so as to be capable of being charged from an on-vehicle generator;  
a diode connected to said battery in parallel in a direction that a forward bias voltage is impressed thereon; and  
a resistor connected to said diode in series.

25 5. A power supply unit as set forth in claim 4, wherein said battery is charged by a charging voltage which is equal to or less than a rated voltage of said battery and which is higher than a forward threshold voltage of said diode.

30 6. A power supply unit as set forth in any one of claims 3 through 5, wherein said diode is a light emitting diode.

35 7. A power supply unit as set forth in claim 6, which further comprises a light receiving element for detecting a light from said light emitting diode to detect an operation state of said light emitting diode.

40 8. A power supply unit as set forth in claim 7, wherein said light emitting diode and said light receiving element form a photocoupler.

45 9. A power supply unit as set forth in any one of claims 1 and 4, wherein said resistor is a variable resistor.

50 10. A power supply unit as set forth in any one of claims 1 and 4, wherein said battery is adopted to be an electric double layer capacitor.

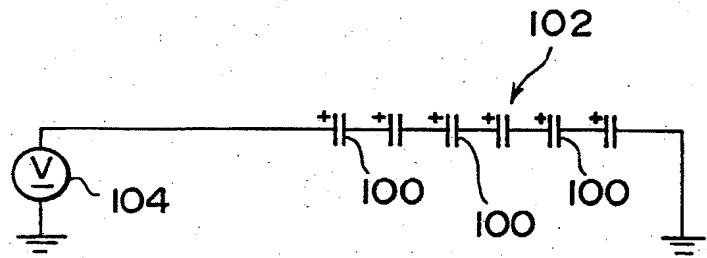


FIG. 1 PRIOR ART

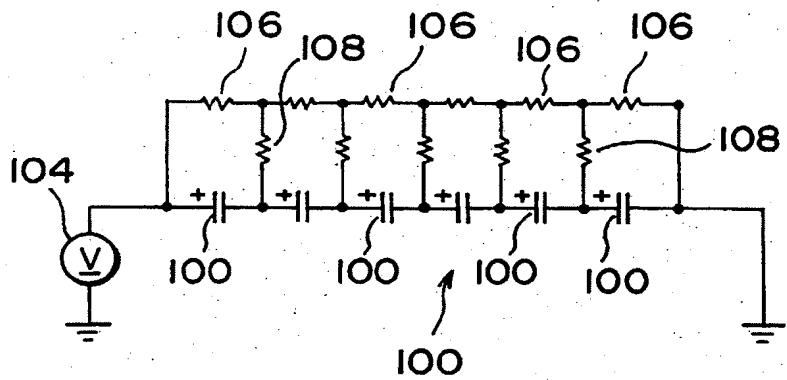


FIG. 2 PRIOR ART

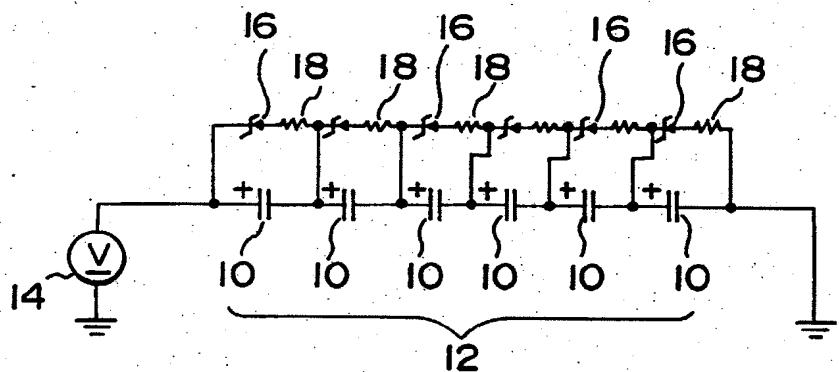


FIG. 3

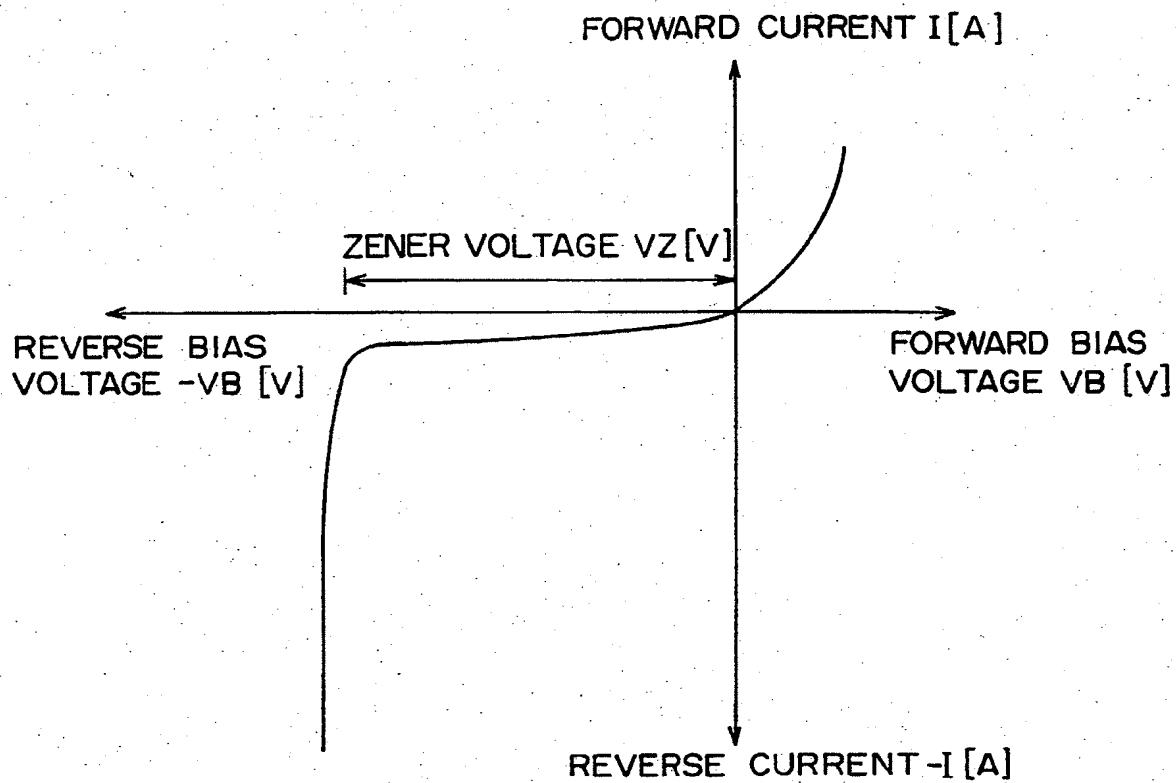


FIG. 4

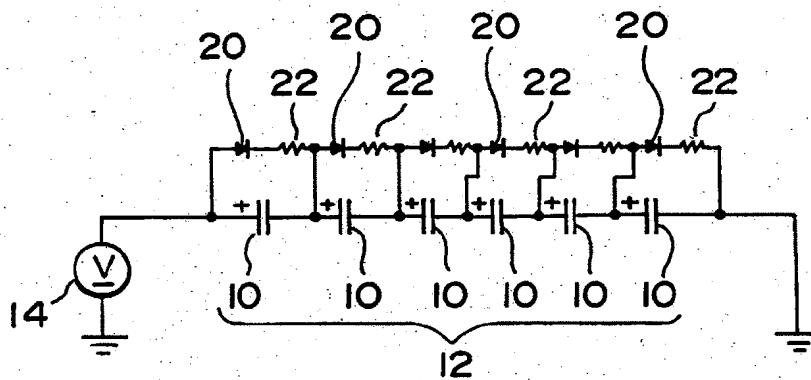


FIG. 5

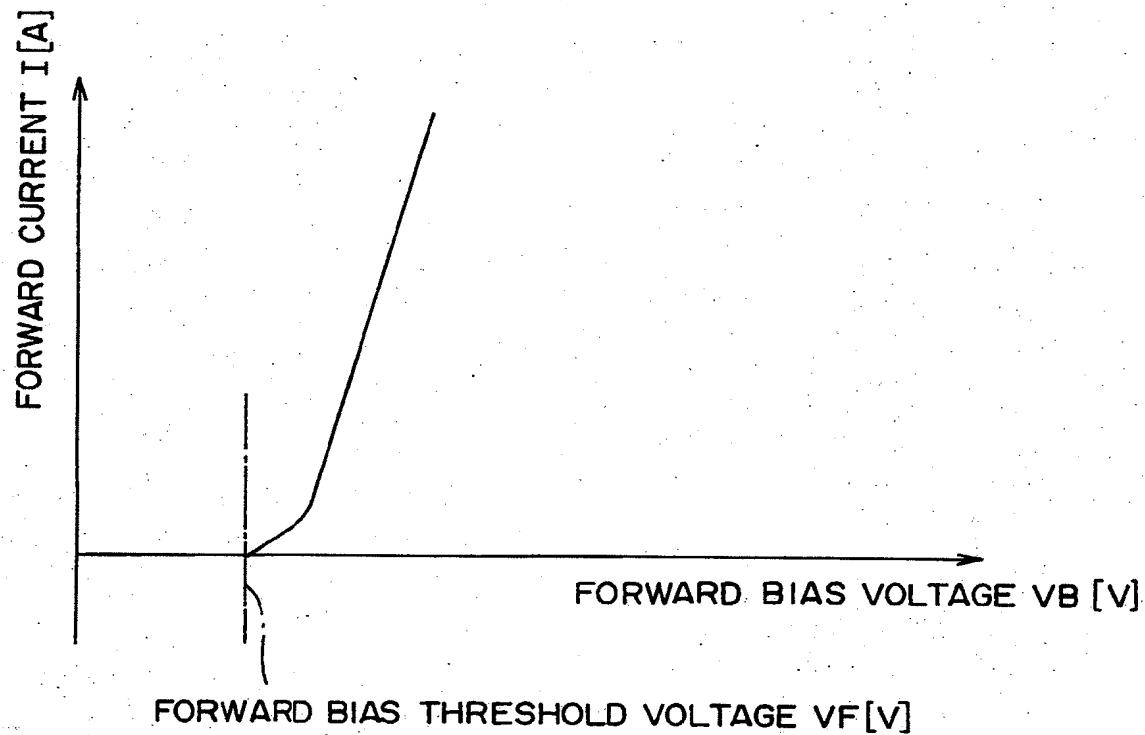


FIG. 6

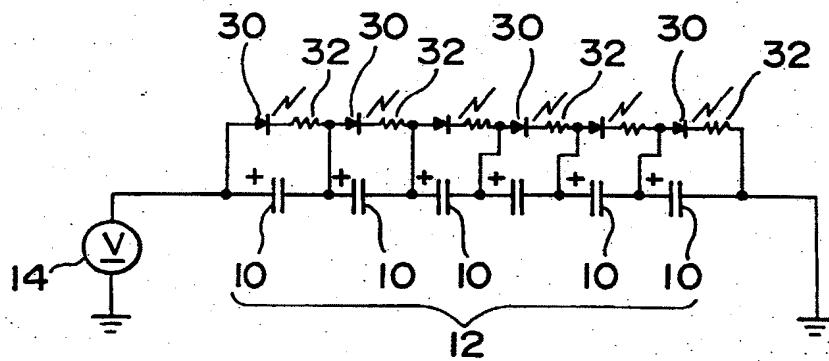
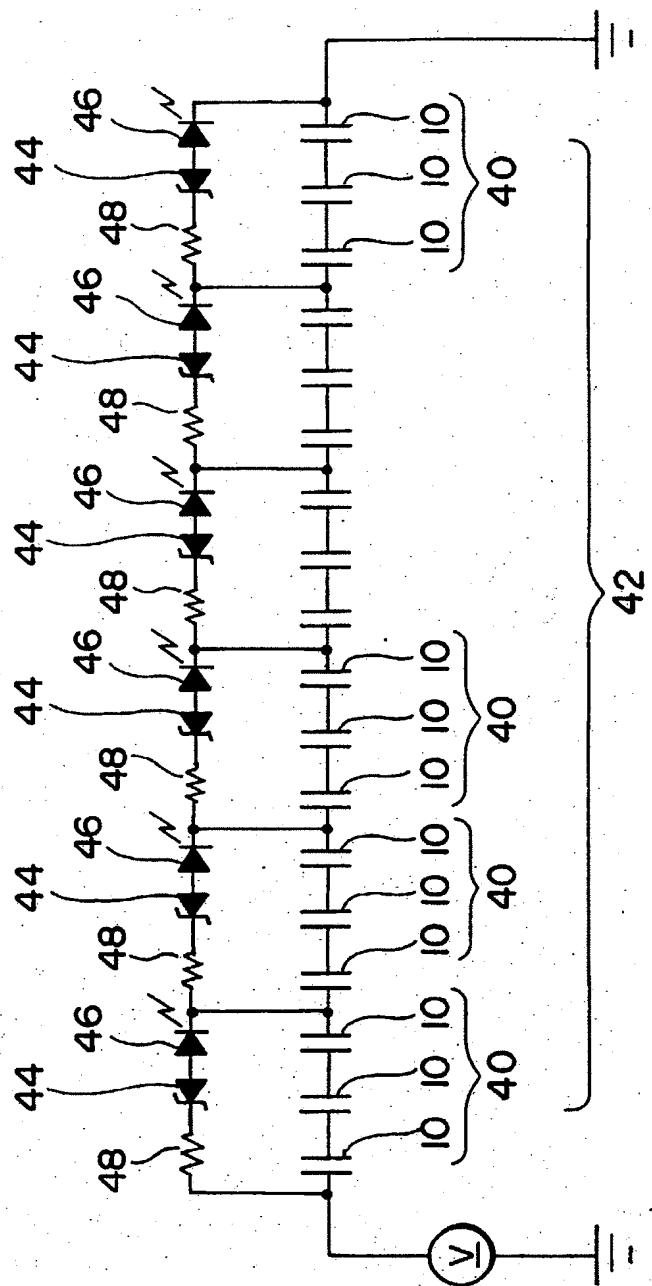


FIG. 7



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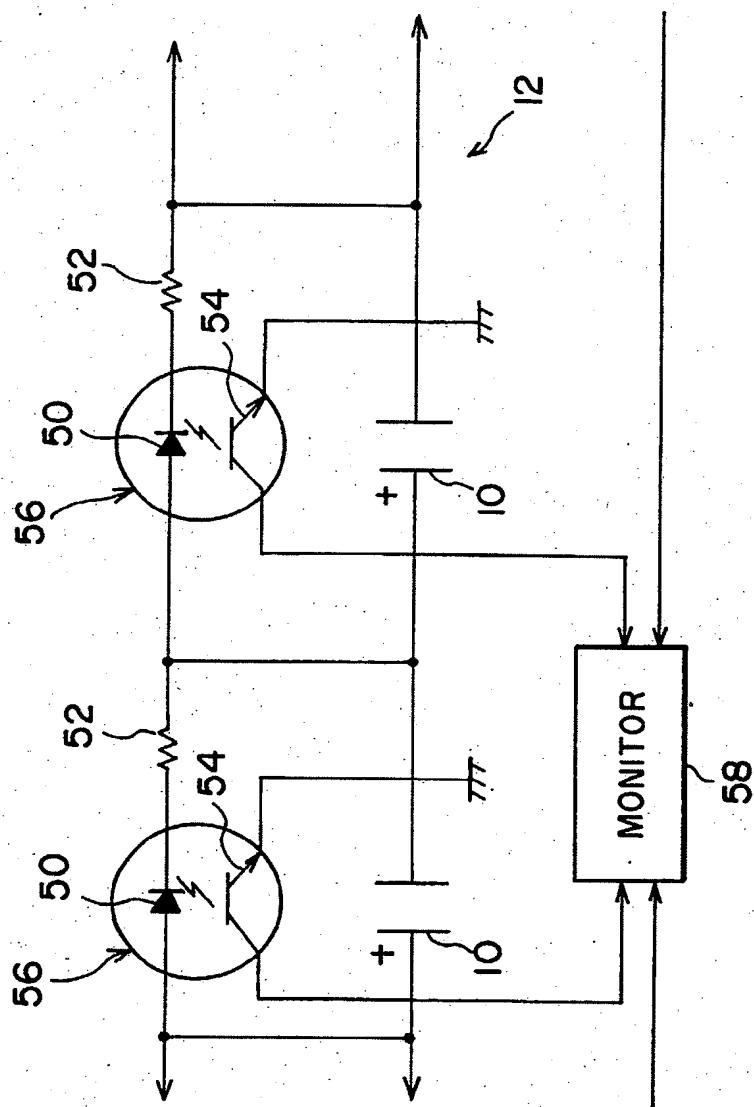


FIG. 9

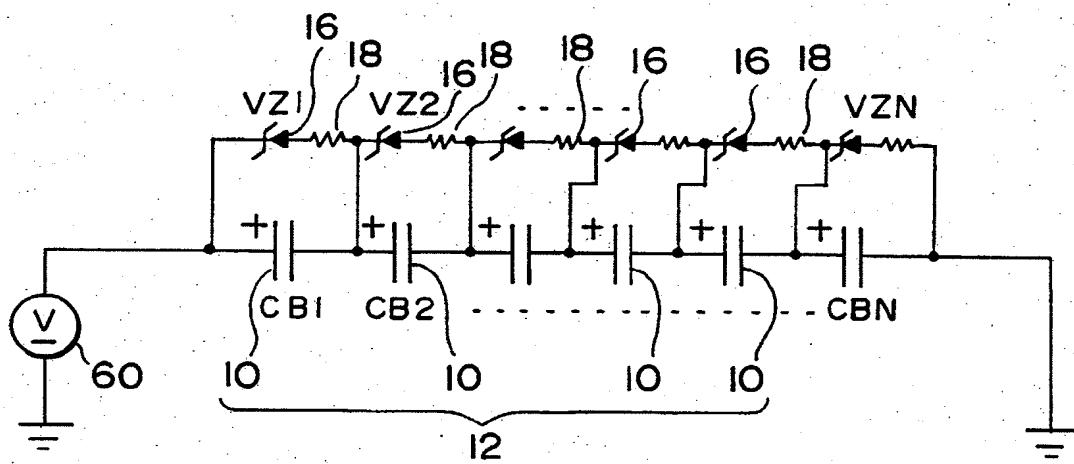


FIG. 10

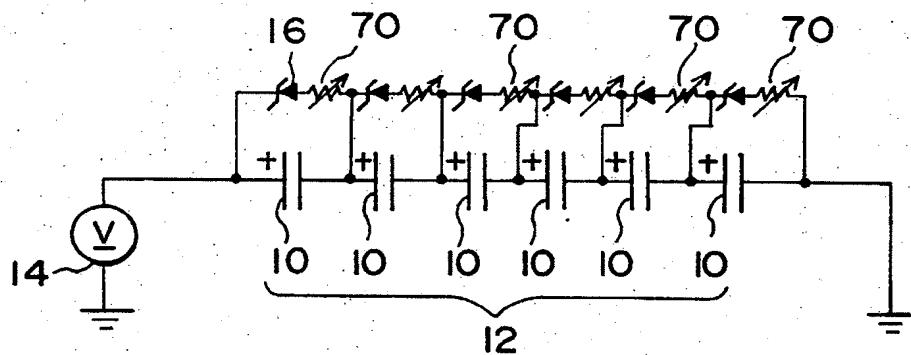


FIG. 11

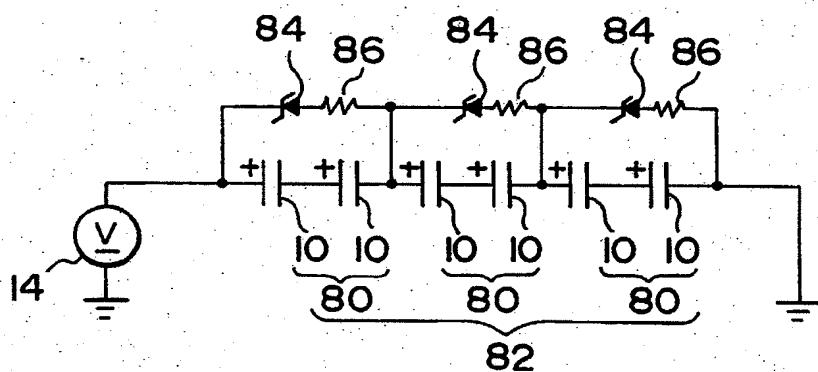


FIG. 12



(19)

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EP 0 795 947 A3

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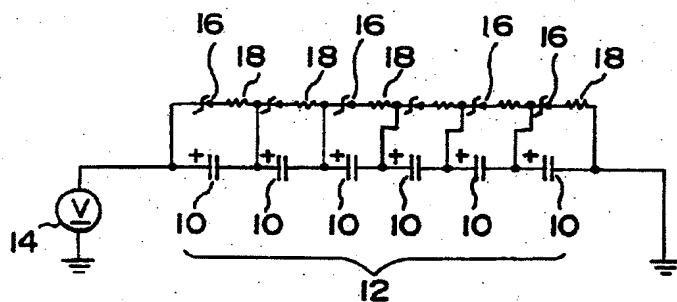
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### (54) Power supply unit for automotive vehicle

(57) A Zener diode 16 is connected to each of single cells 10 of an electric double layer capacitor in parallel, and a resistor 18 is connected to each of the Zener diode 16 in series. Thus, in a case where a single cell 10 is excessively charged, when the bias voltage of the single cell 10 is equal to or higher than the Zener voltage, a discharge current flows through the Zener diode 16

connected to the single cell 10, so that the voltage decreases to the Zener voltage. Thus, it is possible to prevent the electric double layer capacitor from being excessively charged due to the dispersions in electrostatic capacity and internal resistance, and to stably accumulate electricity for a long time.



F I G. 3



DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.6)
Y	US 3 673 486 A (SNEDEKER MARION L) * the whole document *	1,4	H02J7/14 H02J7/00
Y	JASINSKI L: "CHARGERS FOR BATTERIES WITH AUXILIARY CELLS" MOTOROLA TECHNICAL DEVELOPMENTS, SCHAUMBURG, ILLINOIS, US, vol. 8, no. 1, October 1988, page 107/108 XP000001530 * the whole document *	1,4	
A	DE 24 16 897 A (MABUCHI MOTOR CO) * the whole document *	1,4	
A	CH 662 448 A (KERN & CO AG) * the whole document *	1,4	
TECHNICAL FIELDS SEARCHED (Int.Cl.6)			
H02J			
The present search report has been drawn up for all claims			
Place of search	Date of completion of the search	Examiner	
THE HAGUE	13 March 1998	Kelperis, K	
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